

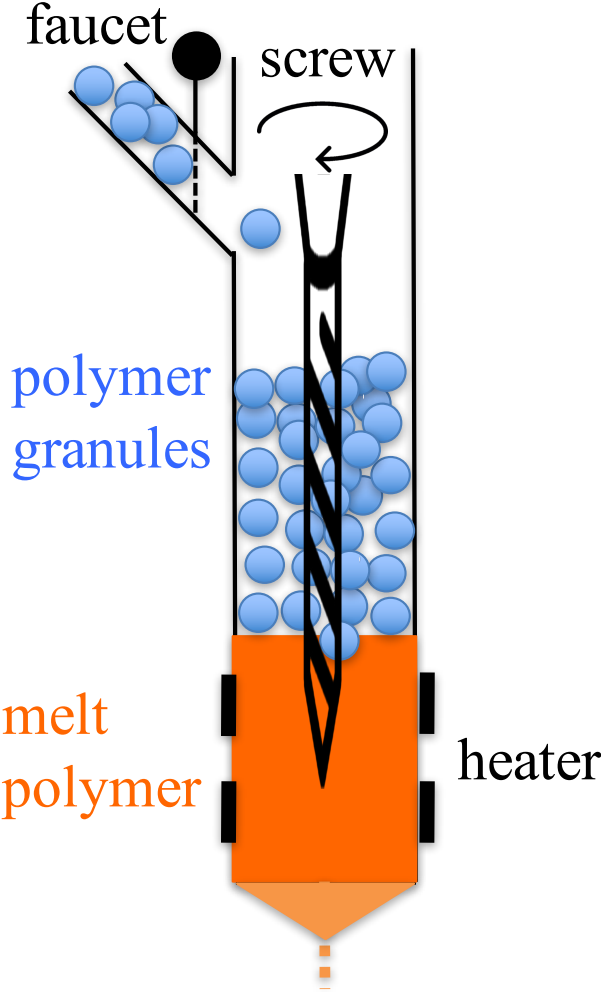
Thermodynamic Modeling and Control of Screw Extruder for 3D Printing

Shumon Koga, David Straub, Mamadou Diagne, Miroslav Krstic

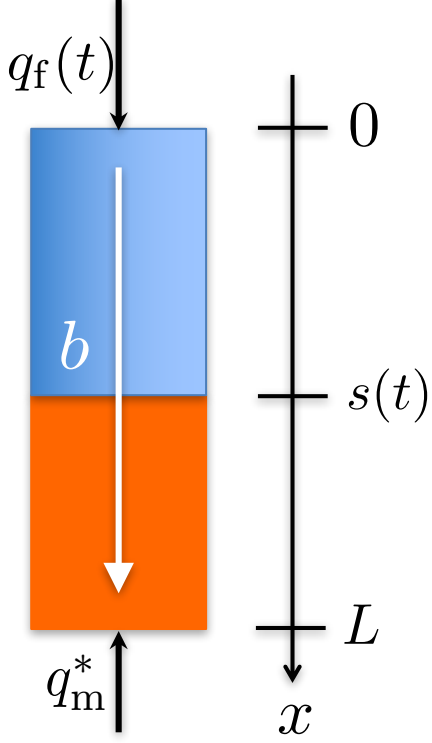
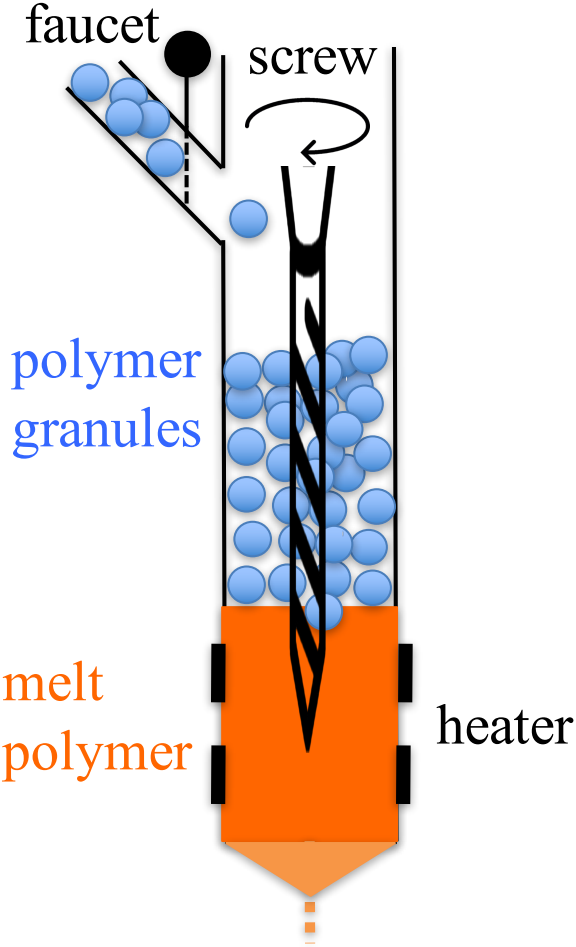
University of California, San Diego

ACC 2018

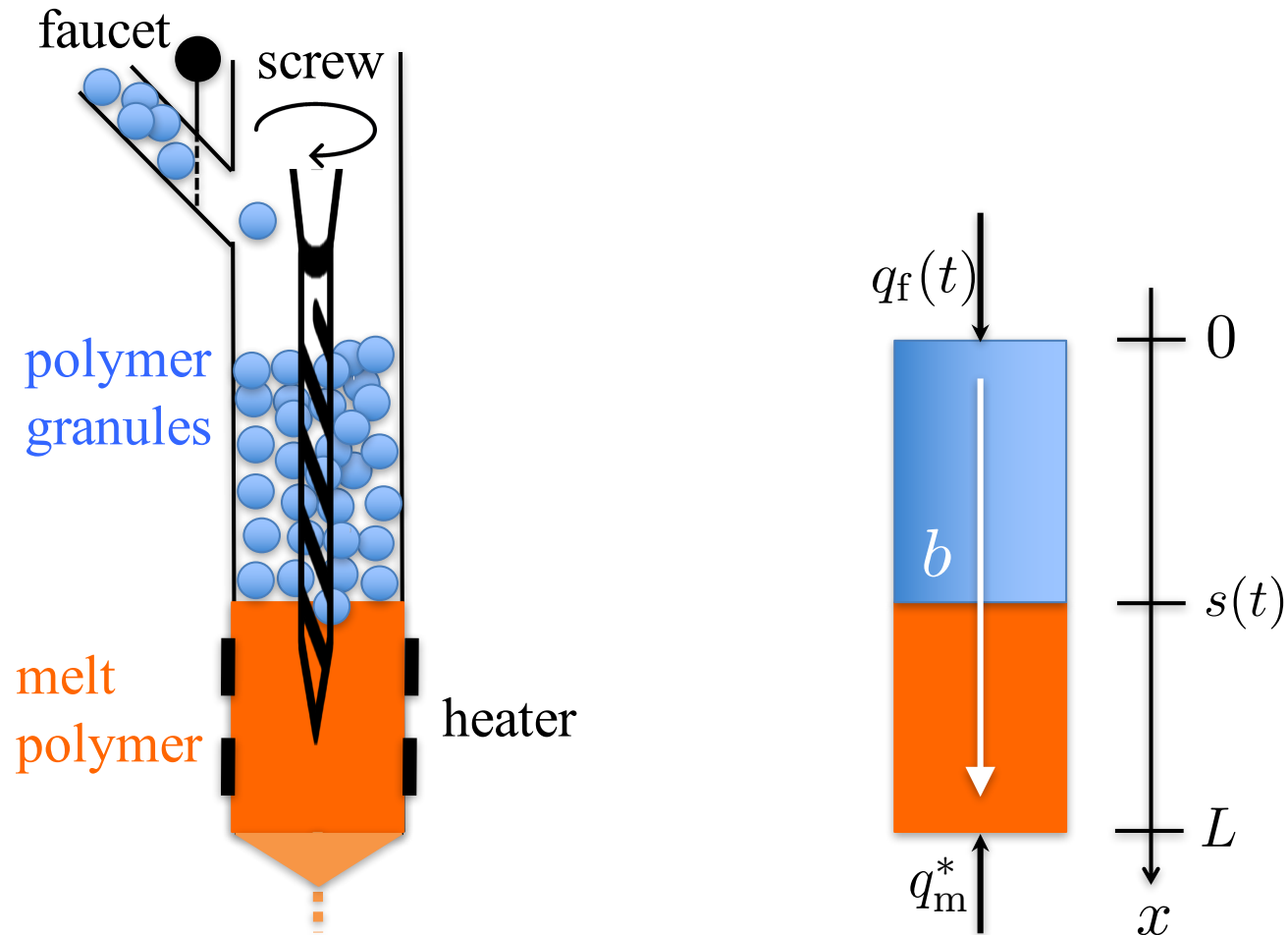
Schematic of Screw Extruder



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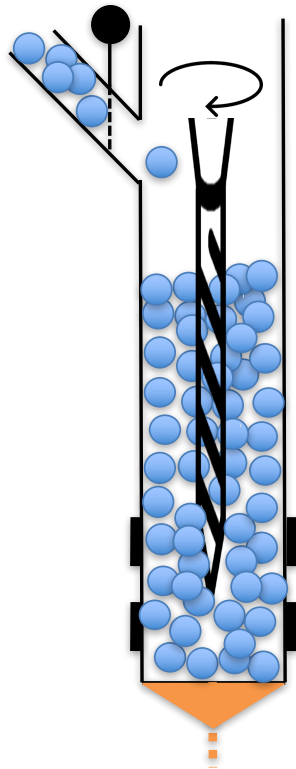
Schematic of Screw Extruder



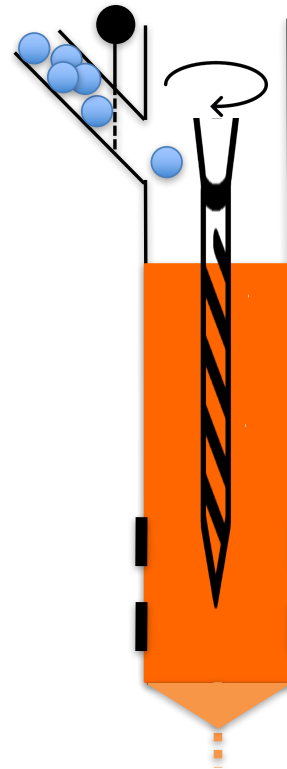
Chosen values : b (extrusion speed), q_m^* (outlet heater), T_b (barrel temp.),

Control : $q_f(t)$ (inlet heat by mixing fed granules with different temperature)

Want to avoid

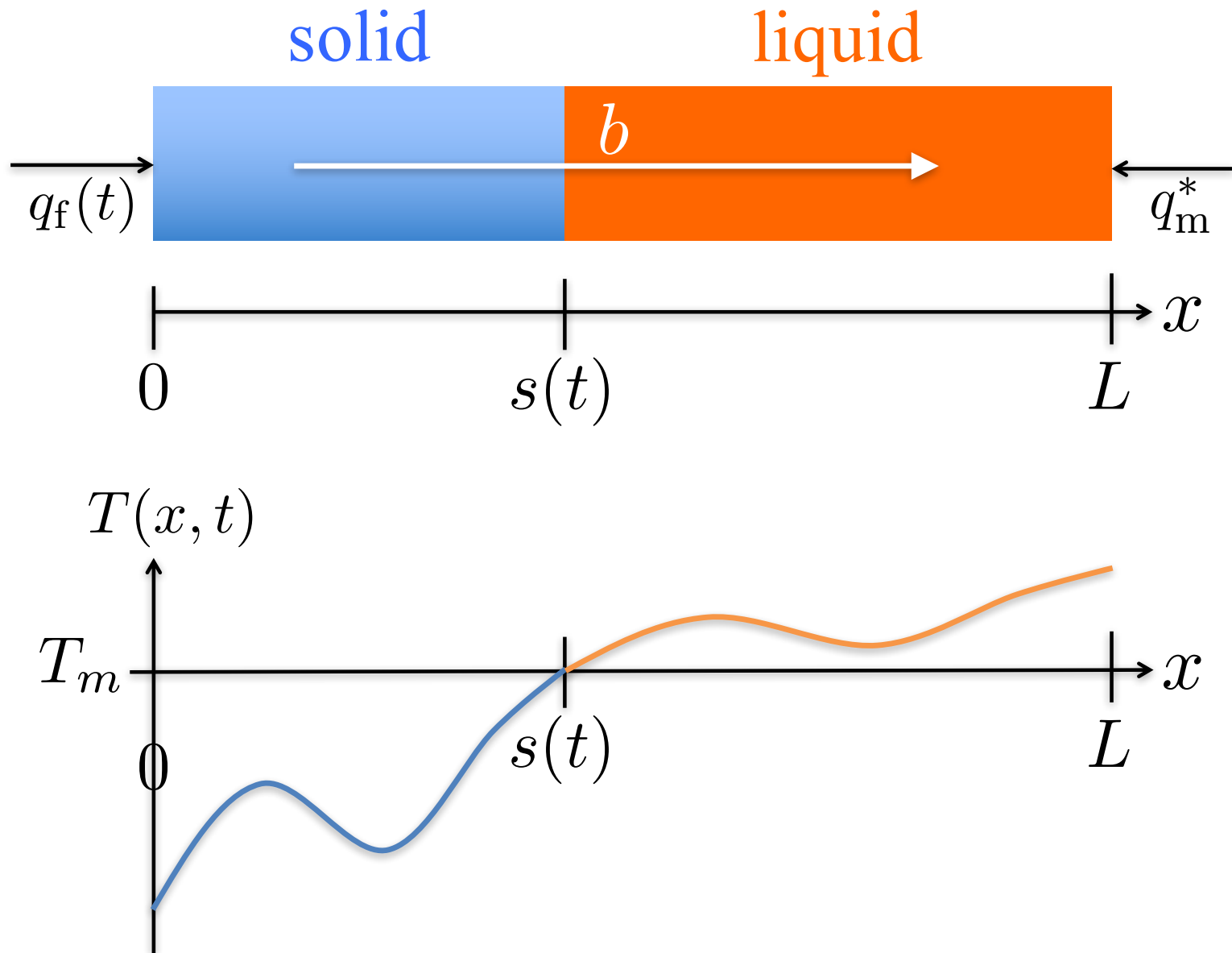


Ink run out



overheating

Problem : Stabilize ratio of granules/melt polymer



Goal : Design cooling heat $q_f(t)$ to achieve $s(t) \rightarrow s_r$.

Thermodynamic Modelling

PDEs (solid & liquid)

$$\frac{\partial T_s}{\partial t}(x, t) = \alpha_s \frac{\partial^2 T_s}{\partial x^2}(x, t) - b \frac{\partial T_s}{\partial x}(x, t) + h_s (T_b - T_s(x, t)), \text{ for } 0 < x < s(t),$$

$$\frac{\partial T_l}{\partial t}(x, t) = \alpha_l \frac{\partial^2 T_l}{\partial x^2}(x, t) - b \frac{\partial T_l}{\partial x}(x, t) + h_l (T_b - T_l(x, t)), \text{ for } s(t) < x < L,$$

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BCs

$$\frac{\partial T_s}{\partial x}(0, t) = -\frac{q_f(t)}{k_s}, \quad \frac{\partial T_l}{\partial x}(L, t) = \frac{q_m^*}{k_l}$$

$$T_s(s(t), t) = T_l(s(t), t) = T_m,$$

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ODE (Interface dynamics)

$$\dot{s}(t) = \bar{\beta} \left(k_s \frac{\partial T_s}{\partial x}(s(t), t) - k_l \frac{\partial T_l}{\partial x}(s(t), t) \right)$$

Model valid iff

$$T_s(x, t) \leq T_m, \quad \text{for } \forall x \in (0, s(t)), \quad \forall t > 0$$

$$T_l(x, t) \geq T_m, \quad \text{for } \forall x \in (s(t), L), \quad \forall t > 0$$

Model valid iff

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Steady-State (SS)

$$\begin{cases} T_{l,\text{eq}}(x) = p_1 e^{q_1(x-s_r)} + p_2 e^{q_2(x-s_r)} + T_b, \\ T_{s,\text{eq}}(x) = p_3 e^{q_3(x-s_r)} + p_4 e^{q_4(x-s_r)} + T_b, \end{cases}$$

where p_i & q_i are parameters calculated by known physical values.

★ If $T_b = T_m$ & $q_m^* = 0$, then $T_{s,\text{eq}}(x) = T_{l,\text{eq}}(x) = T_m$.

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★ If $T_b = T_m$ & $q_m^* = 0$, then $T_{s,\text{eq}}(x) = T_{l,\text{eq}}(x) = T_m$.

Lemma : If the barrel temperature satisfies

$$T_m - \underline{q} \leq T_b \leq T_m + \bar{q}$$

where \underline{q} & \bar{q} are parameters calculated by known physical values, then

$$T_{s,\text{eq}}(x) \leq T_m \text{ \& } T_{l,\text{eq}}(x) \geq T_m.$$

Assumption : Liquid temperature is at SS, i.e., $T_l(x, t) = T_{l,eq}(x)$

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Reference Error States

$$u(x, t) = k_s(T_{s,eq}(x) - T_s(x, t)), \quad X(t) = s(t) - s_r$$

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$$\frac{\partial u}{\partial x}(0, t) = -U(t), \quad u(s(t), t) = k_s(T_{s,eq}(s(t)) - T_m),$$

$$\dot{X}(t) = -\bar{\beta} \frac{\partial u}{\partial x}(s(t), t) + \bar{\beta} (k_s T'_{s,eq}(s(t)) - k_l T'_{l,eq}(s(t))),$$

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Linearize **blue eq.** around $s(t) \approx s_r$.

Linearized Reference Error System

$$\frac{\partial u}{\partial t}(x, t) = \alpha_s \frac{\partial^2 u}{\partial x^2}(x, t) - b \frac{\partial u}{\partial x}(x, t) - h_s u(x, t),$$

$$\frac{\partial u}{\partial x}(0, t) = -U(t), \quad u(s(t), t) = C X(t),$$

$$\dot{X}(t) = A X(t) - \bar{\beta} \frac{\partial u}{\partial x}(s(t), t),$$

where C & A are obtained by known values, and $C > 0$.

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$$\dot{X}(t) = AX(t) - \bar{\beta} \frac{\partial u}{\partial x}(s(t), t),$$

where C & A are obtained by known values, and $C > 0$.

Backstepping Transformation

$$w(x, t) = u(x, t) - \frac{\bar{\beta}}{\alpha_S} \int_x^{s(t)} \phi(x - y) u(y, t) dy - \phi(x - s(t)) X(t),$$

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$$w(x, t) = u(x, t) - \frac{\bar{\beta}}{\alpha_s} \int_x^{s(t)} \phi(x-y) u(y, t) dy - \phi(x-s(t)) X(t),$$

Target System

$$\begin{aligned}\frac{\partial w}{\partial t}(x, t) &= \alpha_s \frac{\partial^2 w}{\partial x^2}(x, t) - b \frac{\partial w}{\partial x}(x, t) - h_s w(x, t) \\ &\quad + \dot{s}(t) \phi'(x-s(t)) X(t), \quad 0 < x < s(t)\end{aligned}$$

$$\frac{\partial w}{\partial x}(0, t) = \frac{b}{2\alpha_s} w(0, t), \quad w(s(t), t) = CX(t),$$

$$\dot{X}(t) = (A - c) X(t) - \bar{\beta} \frac{\partial w}{\partial x}(s(t), t),$$

Control law (derived by transformation & target system)

$$U(t) = -\frac{b}{2\alpha_S}u(0, t) - \frac{\bar{\beta}}{\alpha_S} \int_0^{s(t)} f(x)u(x, t)dx - f(s(t))X(t),$$

where $f(x) = \phi'(-x) - \gamma\phi(-x)$.

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Theorem : Under $T_b = T_m$ & $q_m^* = 0$, the control law makes the closed-loop system **exponentially stable** in the norm $\|T_S(x, t) - T_{S,eq}(x)\|_{\mathcal{H}_1}^2 + (s(t) - s_r)^2$

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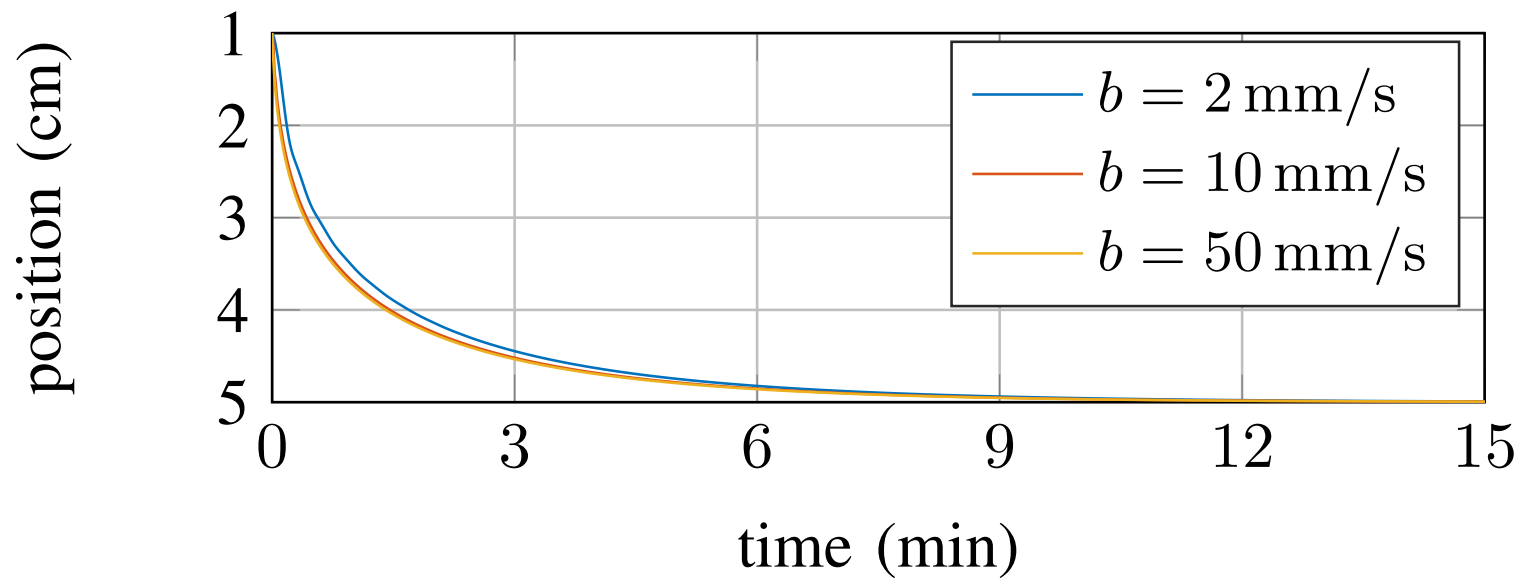
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Apply the designed control to the original two-phase model in numerical simulation

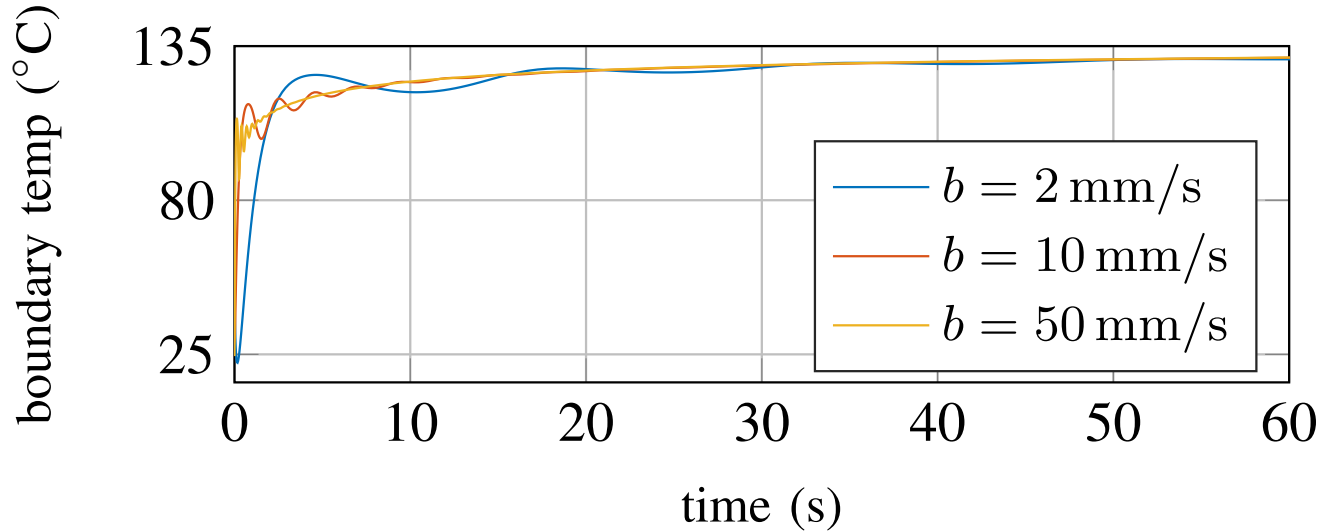
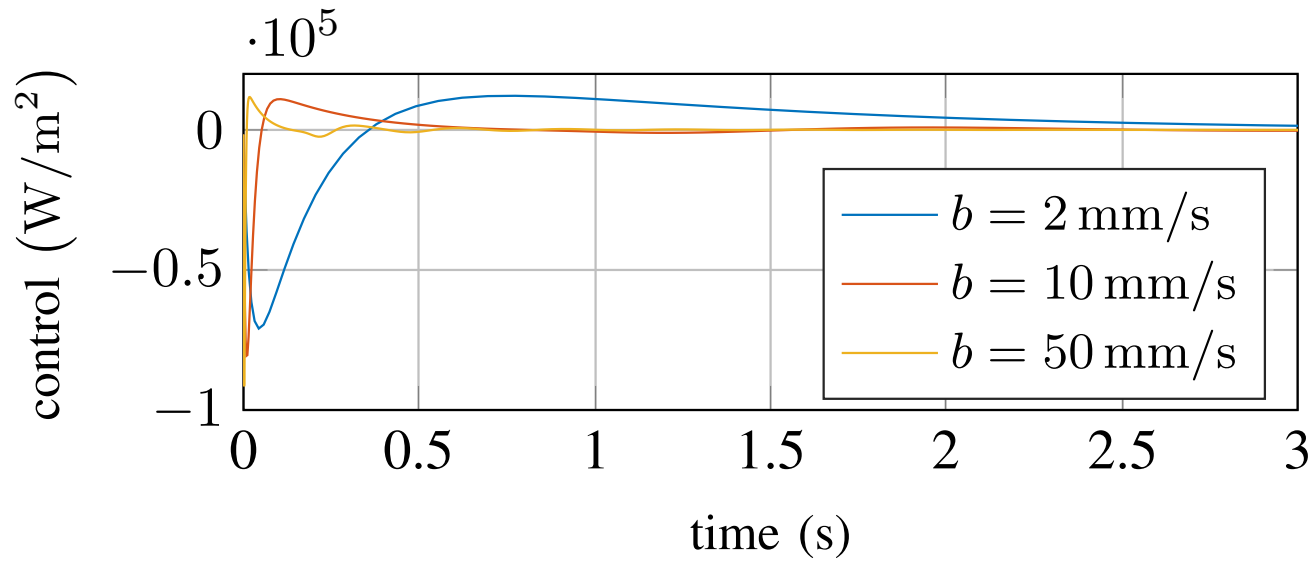
Numerical Simulation

$L = 10$ [cm], $s_r = 5$ [cm],

$T_b = 145$ [°C], $T_m = 135$ [°C], $q_m^* = 100$ [W/m²]



Numerical Simulation



The boundary temperature remains a reasonable value

Future Work

- Observer-based output feedback control
- Relax assumption of $T_l(x, t) = T_{l,eq}(x)$, and design for two-phase dynamics
- Experimental verification of thermodynamic model